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Modeling of Vibrating Atomic Force Microscope's Cantilever within Different Frames of Reference

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• Objective

 Put up FEM based models for the simulation of cantilever vibration modes as tools for the on going work at the AFM – group in AMiR

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 Assess the feasibility of simulating cantilever beams in accelerated frames of reference

Field of research of this group includes among others:

- Manipulation by Lateral Cantilever Vibrations and Oscillations for AFM based nanohandling
- Automation of AFM based nanomanipulation

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Assembled Geometry Objects



- Components were designed using Autodesk Inventor and imported into the COMSOL environment using the *CAD import tool*.
- Details of various components:
 - Cantilever: Single crystalline silicon (450 µm X 50µm X 2µm).

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- Piezo plate: Material PIC155







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a. Inertial Frame Model

- Components: The chip, cantilever, holder and the piezo plate
- Excitation with 0.5 V across the piezo plate; frequency f = 13600 Hz
- Two mechanical and one electrical boundary conditions.
- Multiphysics model: stress-strain and the piezo domain from the MEMS module.

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b. Accelerated Frame Model

- Aims at simplification of the simulation process.
- Components: The chip and the cantilever beam
- Multiphysics model: Only stress-strain domain
- Frequency response implemented in MatLab.
- One mechanical boundary condition.
- Sought Variables:
 - displacements *u*, *v* and *w*
 - from the normal stress ($\boldsymbol{\varepsilon}$) and strain ($\boldsymbol{\gamma}$) a).



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Relationship between Vertical Coordinates (z,z*):

$$z$$
 = $z^* + Asin(\omega t)$

Newton's Second Law:

 $m\ddot{z}$

$$= m\ddot{z^*} - mA\omega^2\sin(\omega t)$$

 $\rho := m/V$

Fictitious Force:

$$F_z^* := F_z + mA^2 \sin(\omega t) = m\ddot{z^*}$$

Fictitious Load:

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$$L_f := \rho A \omega^2 \sin(\omega t) ;$$

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Vibration Amplitude





Simulation of the actuation system:

• Frequency Response

- Determine the vibration amplitude of the piezo plate at the holder (Frequency = 13600 Hz and Voltage = 0.5 V): Result - (A_{sim} = 0.0430 nm)
- Frequency dependent

Eigenfrequency Response

- The 1st 20 eigenfrequencies of the piezo plate and holder (between 5.62x10⁵ 1.12x10⁶ Hz), hence no influence on the cantilever.
- For every eigenfrequency max displacement is shown



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Results from both models



Division of Microrobotics and Control Engineering Prof. Dr.-Ing. habil. S. Fatikow Displacement amplitude at the tip of the cantilever. Resonance peak at the frequency:

 $f_{Mod1} = f_{Mod2} = (13.600 \pm 0.005) \text{ kHz}$

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 This corresponds well with the analytically determined frequency for a clamped-free cantilever beam

 $f_{theo} = 13.586 \ kHz$

and the frequency specification range stated by the manufacturer

 $f_{Manu} = 13 \pm 4 \ kHz$

Simulation time for both models (CPU time):

$$T_{Mod1} = 3.375 * T_{Mod2}$$

Conclusion

Discussion

- Simulation of cantilever's vibration modes, when implemented in suitably chosen frames of reference can:
 - Help reduce computational burden
 - Shorten calculation time
- Results for the resonance frequency agree within ± 5 Hz.
- Lack of damping leads to resonance catastrophe, thus no comparison amplitude possible in this case

Outlook

- Implementation of damping
- Comparison of amplitude values with experimental results



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