## Partial discharge risk under space charges generation and transport effects

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## STUDY CONTEXT AND PROBLEMATIC

# COMSOL® IMPLEMENTATION & SIMULATION MODEL

# MAIN SIMULATION RESULTS



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(1) Electronics components

**2** Power Converters

Busbars powered by a HVDC 2.5kV voltage bus









## Study context and problem - Charge generation in dielectrics materials





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A better characterization of charge mechanisms in dielectrics material to prevent partial discharge risk in air surrounding HVDC power systems.

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#### Implementation under Comsol (1/2) - Simulation conditions

## Geometry and meshing

2D-simulation model

162 k domain elements ~4 M Finite elements

Interfaces refinement 50 Boundary layers

**∂**V=0 3 Air Air 2.5 ∂(εE)=ρ ∂(εE)=ρ ∂(εE)=ρ **y-position** (mm) (mm) **y ∂V**=0 **∂V=**0 Cathode (0 kV) Anode (2.5 k 0.5 Dielectrics (PTFE) 0 x-position (mm) -2 3 -1 2 1

## Initial conditions

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#### Initial charge and associated Potential distribution **Electric field distribution** Time=0 min Electric 0.02 0.3 Space charge density (C.m<sup>-3</sup>) potential (V) y-position (mm) 5.2 1 2 1 2 1 0.00 0 0.2 Electric field (kV/mm) -0.02 -50 0.1 -0.04 -100 0.0 -0.06 -150 -0.1 -0.08 -200 -0.2 0.5 -0.10 Cathode Anode -250 -0.12 -0.3 0.0 0.2 0.4 0.6 0.8 1.0 -1 2 0 1 x-position (mm) x-position (mm) Triple points Laplace

## Initial conditions

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#### Main model equations

• Poisson equation :  $\frac{\partial E(x,y)}{\partial x \partial y} = \frac{\rho(x,y)}{\varepsilon_r \varepsilon_0}$ 

• Transport equation 
$$j(x,t) = n(x,t) \cdot \mu(E,t) \cdot E(x,t)$$

• Continuity equation :  $\frac{\partial \rho}{\partial \rho}$ 

$$\frac{\partial \rho(x,t)}{\partial t} + \frac{\partial j(x,t)}{\partial x} = s(x,t)$$



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## 🖙 With

• j(x,t) the injection/extraction at interfaces  $: J(x,t) = AT^2 \exp\left(-\frac{qW_{e,h}}{k_pT}\right) \exp\left(\frac{q}{k_pT}\right) \sqrt{\frac{qE(x,t)}{4\pi\varepsilon}} - 1$ 



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- $\mu(E,t)$  Charge mobility as function of E(x,t) :

$$\mu(E,t) = \frac{2\lambda v}{E(x,t)} \left[ \exp\left(-\frac{\phi_a}{k_B T}\right) \right] \sinh\left(\frac{q\lambda E(x,t)}{2k_B T}\right)$$



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#### 11 variables to compute for model solving - Implementation under General-PDE modules

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 $[ (P, T^{\circ}) = (1,013 \text{ bar, } 20^{\circ}\text{C});$ Uniforme electric field /air gap; Plane electrodes;

$$U_{p} = \frac{B \cdot (pd)}{\ln(pd) + \frac{A}{\ln\left(1 + \frac{1}{\gamma}\right)}}$$
$$A_{air} \approx 15 \text{ (Torr}^{-1}.\text{cm)}$$

$$B_{air} \simeq 365 (V.Torr^{-1}.cm^{-1})$$
  
 $\gamma = \frac{n_{secondary}}{N}$ 



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<sup>[1]</sup> F. Paschen Über die zum Funkenübergang in Luft, Wasserstoffand Kohlensäure bei verschiedenen Drücken erforderliche Potentialdifferenz, Wied. Annalen der Physik und Chemie. Wiede-manns Annalen, Ser. 3, **37**(1), 69 (1889)

#### Electric field at triple points

- $E_{max}(x, t)$  decreases by 72% at anode triple point and increases by 4% at cathode triple point ;
- Implanted charges disturb the electric field distribution in dielectrics;
- $|E_{max}(x,t)|$  in air  $\geq 3 \ kV/mm$  ;

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#### Partial discharge risk at triple points.



Charge injection mechanism at triple points

 More holes injection from anode than electrons from cathode;

- Each charge type increases with time at both interfaces;
- Low trapping and transport mechanisms in the bulk with time ;

The nature and distribution of injected charges has a significant impact on partial discharge risk at triple points.



#### Conclusion

Simulated Model giving well agreement with experimental measurements for LDPE material



Confrontation with PTFE experimental measurements

Use of Powerful Comsol<sup>®</sup> solver to compute the model more quickly than Fortran<sup>®</sup> source code



# THANK YOU FOR YOUR ATTENTION

