

**INTRODUCTION:** All vanadium redox flow batteries (VRFB) typically consist of planar cells with flow-by fluid flow design [1]. Their limiting current densities are determined by electrolyte convection in porous electrodes [2]. The key parameters flow channel depth and hydraulic permeability  $\kappa$  of the porous electrode depend on electrode compression and are difficult to measure directly. In this study both parameters are determined from experimental VRFB cell data by analytical approximations. Parametrized models and parameters are validated in order to enable simulations of alternative cell designs such as interdigitated fluid flow [1] or tubular cells [3].

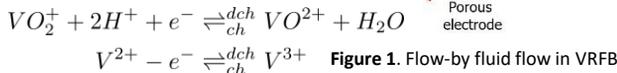
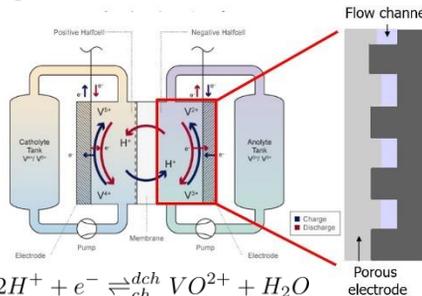


Figure 1. Flow-by fluid flow in VRFB

**EXPERIMENTAL:** A planar VRFB cell with 20 parallel flow channels ( $w_f = 0.10$  cm,  $w_p = 0.20$  cm,  $l_f = 5.0$  cm) is used to measure pressure drops and polarization curves for cell flow rates  $Q = 0.5$  ml/min - 40 ml/min with vanadium concentration 1.6 mol/l at SoC = 90%.

**COMPUTATIONAL METHODS:** Stationary studies in the COMSOL free and porous media flow module were performed using Navier-Stokes equations for the flow

$$FC \quad \rho(\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla p + \mu \Delta \mathbf{u} \quad \nabla \cdot \mathbf{u} = 0$$

$$PE \quad \frac{\rho}{\epsilon^2}(\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla p + \frac{\mu}{\epsilon} \Delta \mathbf{u} - \frac{\mu}{\kappa} \mathbf{u} \quad \nabla \cdot \mathbf{u} = 0$$

channel (fc) free flow and Brinkmann-Darcy equations for the porous electrode (pe) flow. Periodical boundary conditions were used for the porous electrode cut planes.

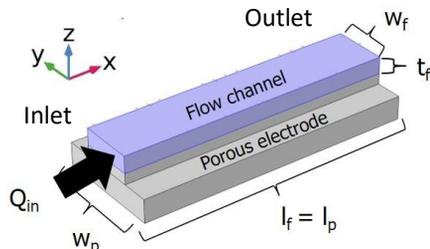


Figure 2. Base configuration – single flow channel

### RESULTS:

#### Parametrization by experimental data

The effective flow channel depth  $t_f$  is fitted from Hagen-Poiseuille pressure drop estimates to experimental values.

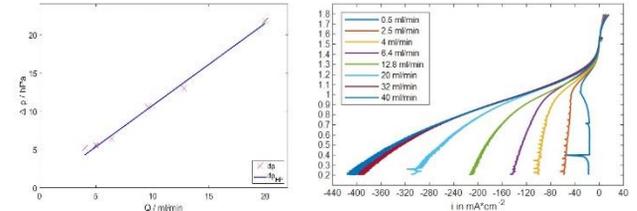


Figure 3. Pressure drops and current densities for flow rates  $Q$

The effective hydraulic permeability of the electrode is fitted by an analytical 1D approximation for the porous electrode flow rate  $Q_p$  [2] and the convection part of the experimental limiting

$$i_{lim,conv} = \frac{F \cdot c_V \cdot SoC \cdot Q_p(Q, \kappa)}{w_p \cdot l_p}$$

current densities.

#### Model and parameter validation

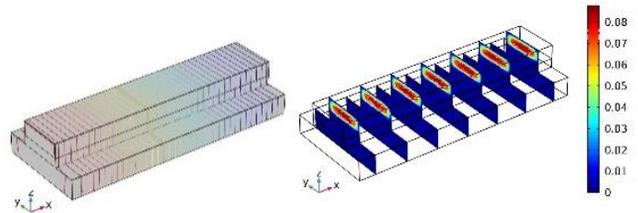


Figure 4. Pressure drop and velocity distribution ( $u$  / m/s) @20 ml/min

$$\Delta p_{sim} = 18.3 \text{ hPa} \quad i_{lim,sim} = 288 \text{ mA/cm}^2$$

$$\Delta p_{exp} = 21.9 \text{ hPa} \quad i_{lim,exp} = 317 \text{ mA/cm}^2$$

Validation results are slightly below experimental values.

#### Simulations

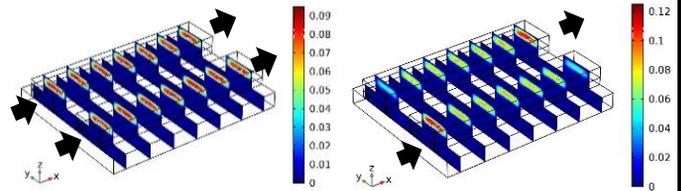


Figure 5. Fluid velocity in parallel (left) and interdigitated flow designs. Simulations for different flow designs can be performed using the model and the parameters from experiment.

**CONCLUSIONS:** Analytical approximations can be used to parametrize fluid flow models from experimental cell data. Simulation results are within 10-20% deviations consistent with experimental values. Future work will concentrate on experiments and simulations for tubular cell designs [3] as well as on electrochemical 3D simulations using the COMSOL batteries and fuel cell module.

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#### REFERENCES:

- L. F. Arenas et al., Redox flow batteries for energy storage: Their promise, achievements and challenges, *Current Opinion in Electrochemistry* 16 (2019), 117-126.
- X. Ke et al., A simple analytical model of coupled single flow channel over porous electrode in VRFB with serpentine flow channel, *Journal of Power Sources* 288 (2015) 308-313
- S. Ressel et al., Performance of a vanadium redox flow battery with tubular cell design, *Journal of Power Sources* 355 (2017) 199-205.