

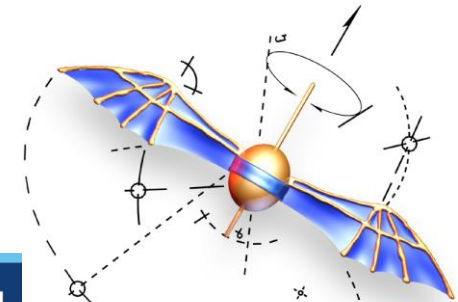
Numerical study of thermal evaporation unit for phase change of liquid hydrogen peroxide to vapor

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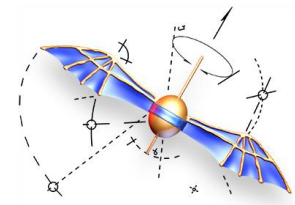
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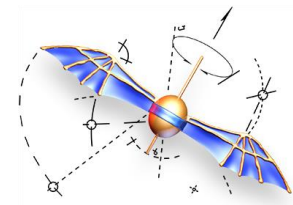


Outline

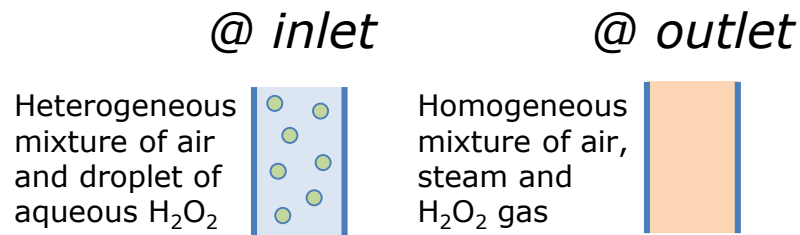


- Introduction and motivation
- Physical background
- Numerical model
- Results
- Conclusions

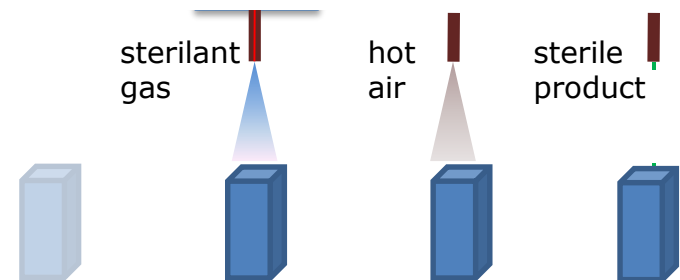
Introduction and motivation



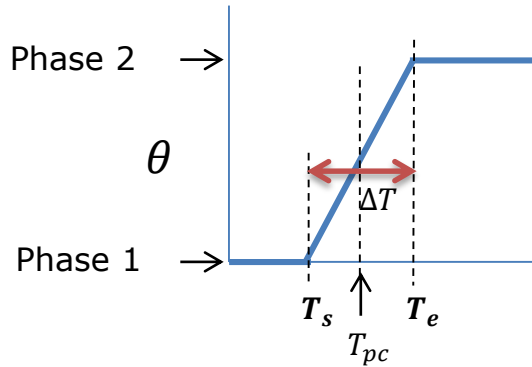
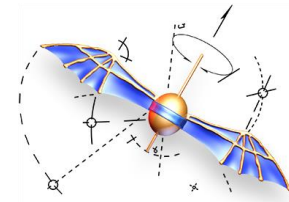
- Hydrogen peroxide (H_2O_2)
 - Strong antimicrobial properties
 - Commonly applied in the form of gas/vapor for package sterilization in aseptic filling machines
 - Gaseous or vapor form is produced by evaporating and subsequent heating of an **aerosol** mixture of aqueous H_2O_2 and air



- Involve high energy and material costs
- Little knowledge about the process
- Slow development



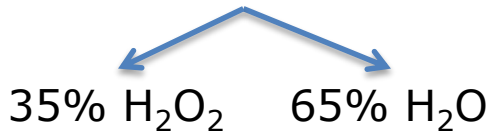
Physical background



Phase fraction: $\theta = \begin{cases} 0: T_{pc} - \Delta T/2 \rightarrow T_s \\ \downarrow \\ 1: T_{pc} + \Delta T/2 \rightarrow T_e \end{cases}$

The equivalent (effective) material properties defined as a function of phase fraction

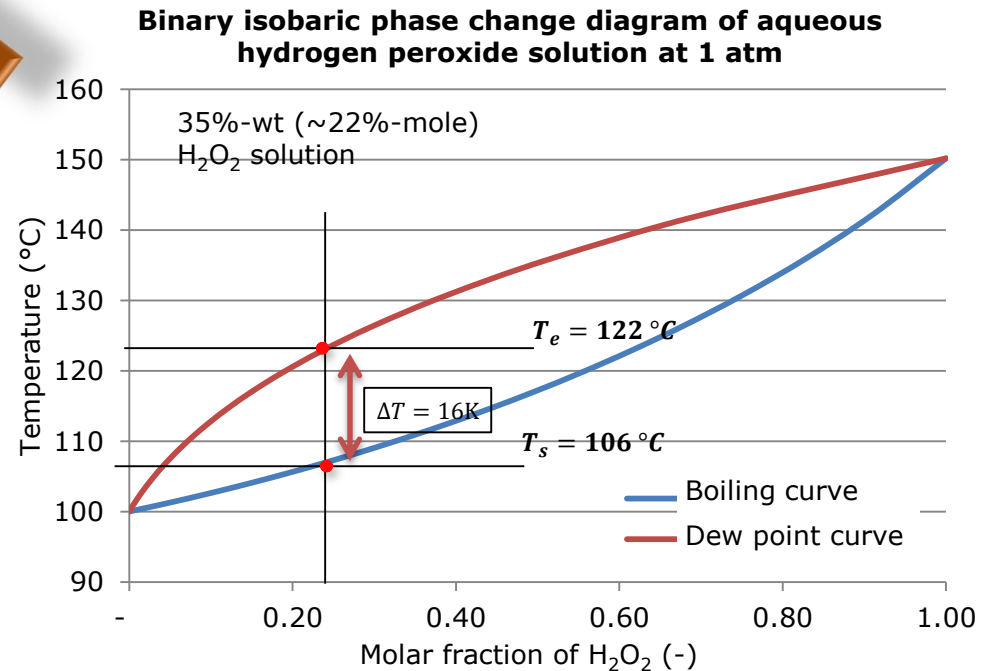
Aqueous H₂O₂ (35%-wt) solution



Binary mixture

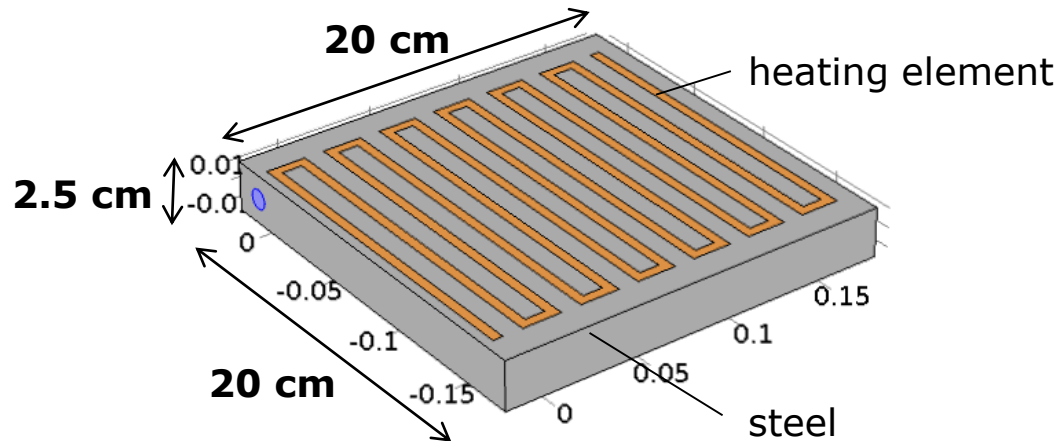
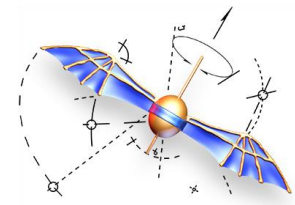
100°C **150°C**

1. Phase change of aerosol mixture
2. Material properties → molar basis
3. Constant H₂O₂ concentration



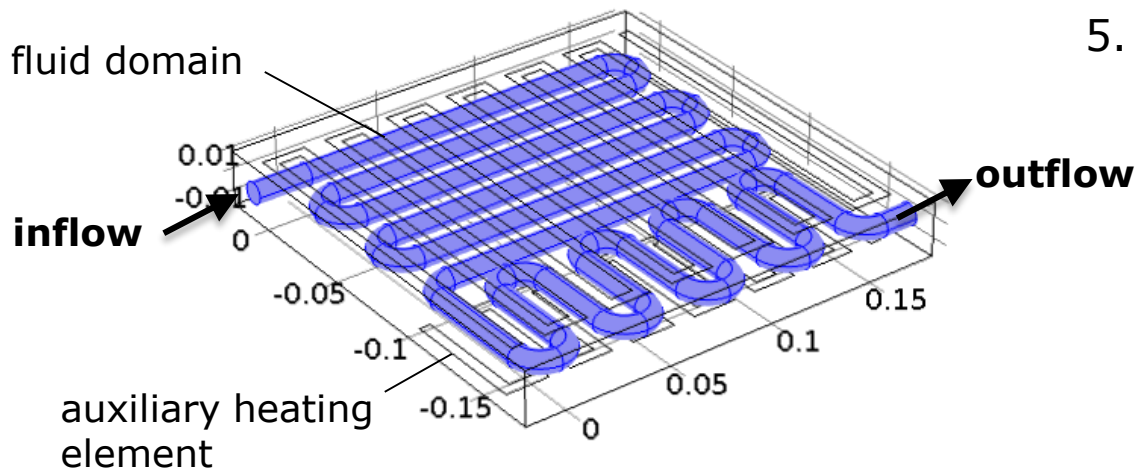
→ Figure based on the formulations published by Scatchard et al. (1952), Keyes (1947) and corrections from Manatt and Manatt (2004)

Numerical model: Geometry and parameters

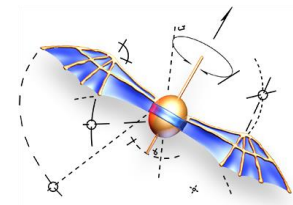


Model parameters:

1. Electric current value
2. H₂O₂ concentration
3. Volumetric flow rate of H₂O₂
4. Volumetric flow rate of air
5. Stop criterion for parametric solver (temperature)



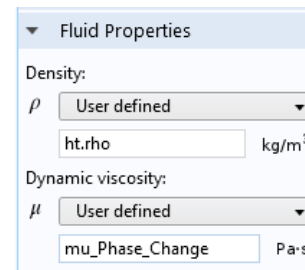
Numerical model: Physical interfaces



The interdependencies:

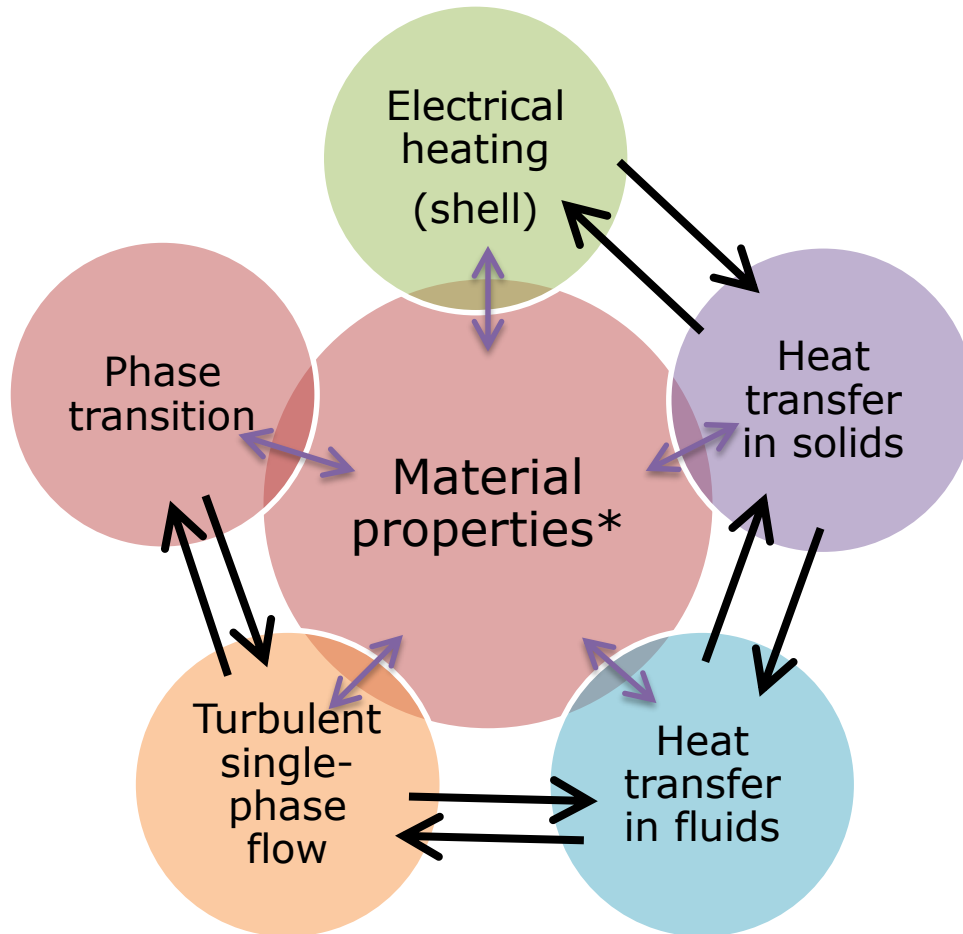
- ▶ Electric Currents, Shell (*ecs*) {*ecs*}
- ▶ Heat Transfer in Fluids (*ht*) {*ht*}
- ▶ Turbulent Flow, Algebraic yPlus (*spf*) {*spf*}

- $Q_s = \mathbf{J} \cdot -\nabla \mathbf{V} \rightarrow$ surface joule heating
- $\nabla_t \cdot (d_s \kappa_s \nabla_t T) = Q_s \rightarrow$ boundary heat source
- Heat transfer to fluid domain
- Temperature change \rightarrow phase fraction (θ) change
- Temperature and phase fraction change \rightarrow flow properties change using:



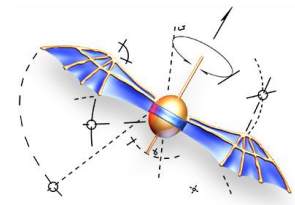
$$\rho = \theta \rho_1 + (1 - \theta) \rho_2$$

$$\mu = \theta \mu_1 + (1 - \theta) \mu_2$$

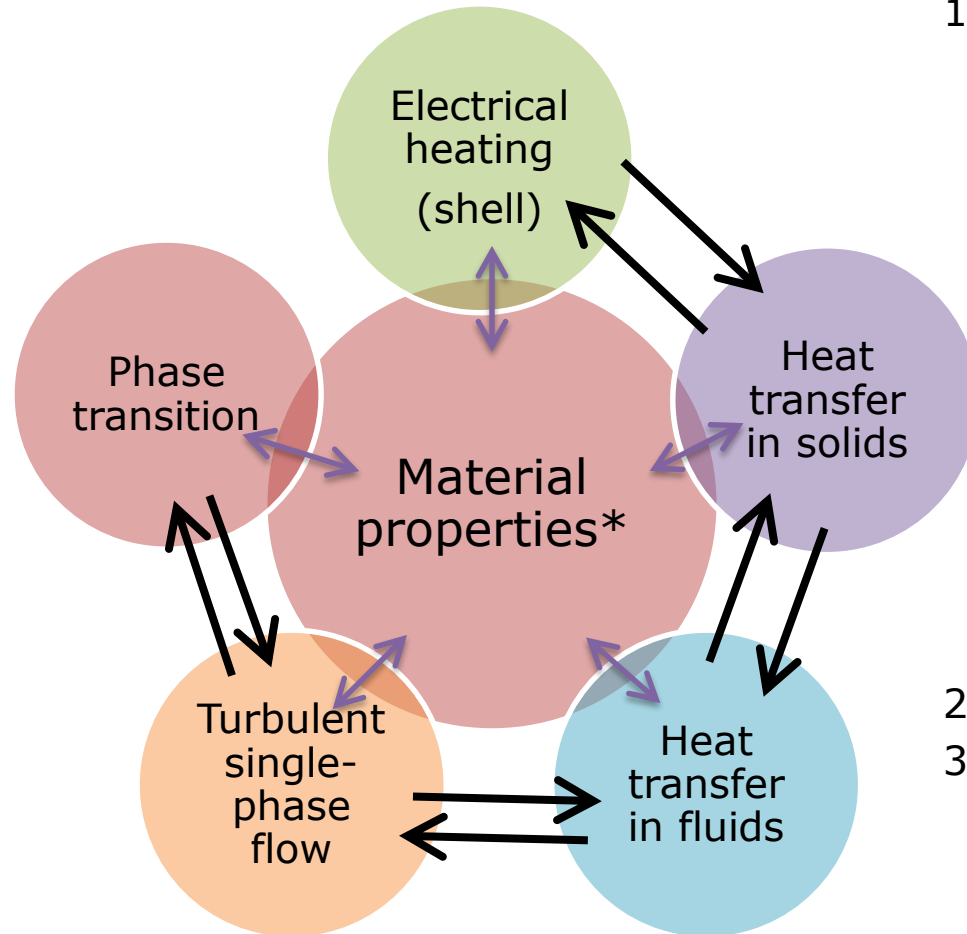


* Aerosol was assumed as an ideal mixture.

Numerical model: Mesh and study



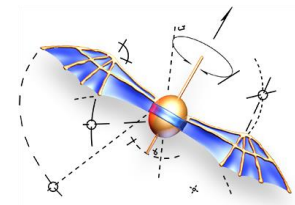
The interdependencies:



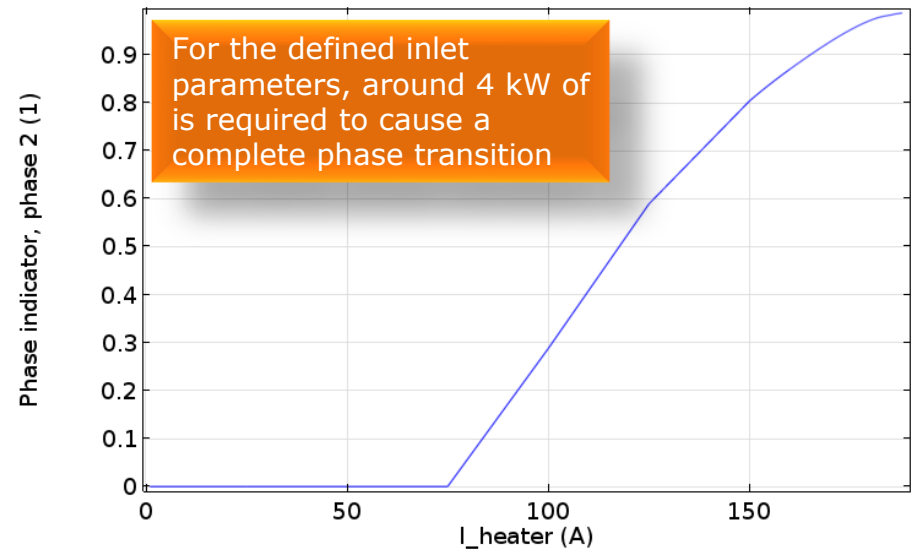
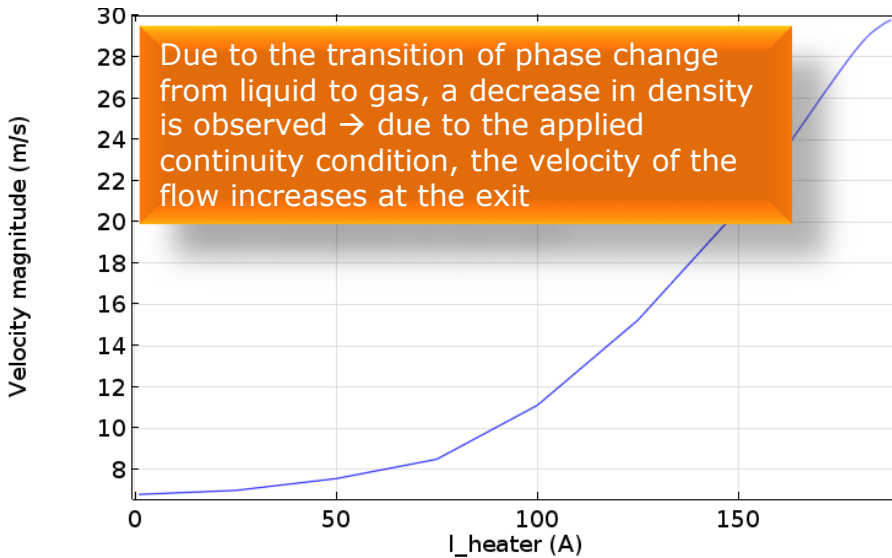
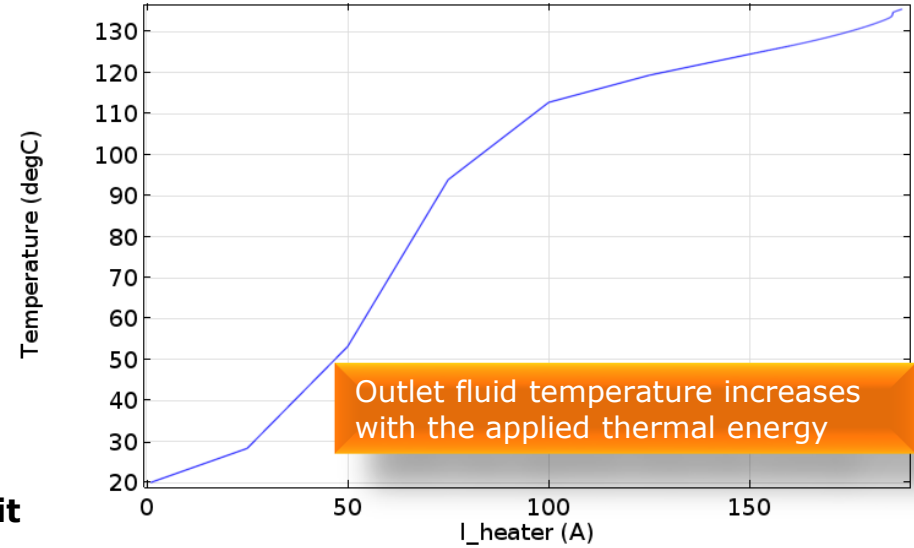
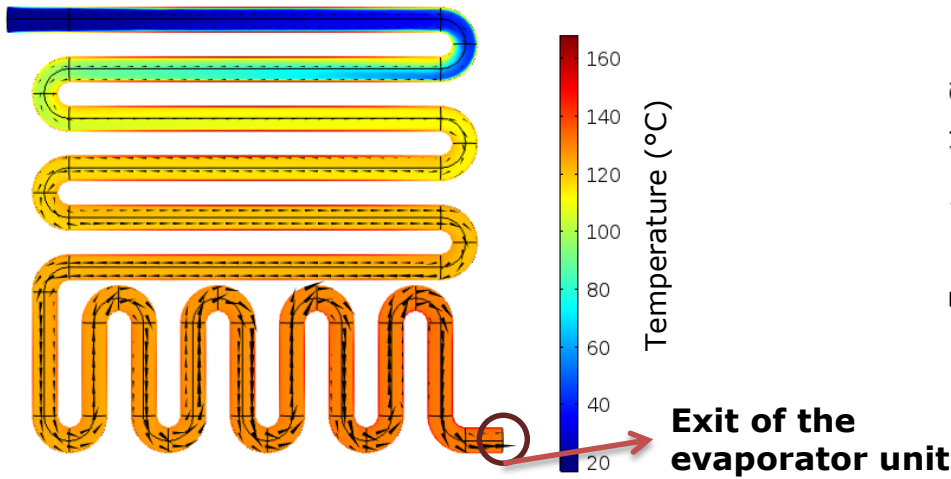
* Aerosol was assumed as an ideal mixture.

1. Steady state solution
 - **Study 1:** Initial guess → isothermal flow defined at the inlet temperature
 - **Study 2:** Auxiliary parametric solver (with continuation) for the electric current (coarse values), while plotting the average phase indicator of fluid 2 at the outlet.
 - **Study 3:** Using last converged value from Study 2 as initial condition for fully coupled solver and a small range for the parametric solver
2. Direct solvers are used → robustness
3. Coarse mesh with quadratic discretization level for heat transfer was used → faster convergence

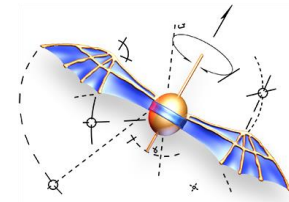
Results: Phase change



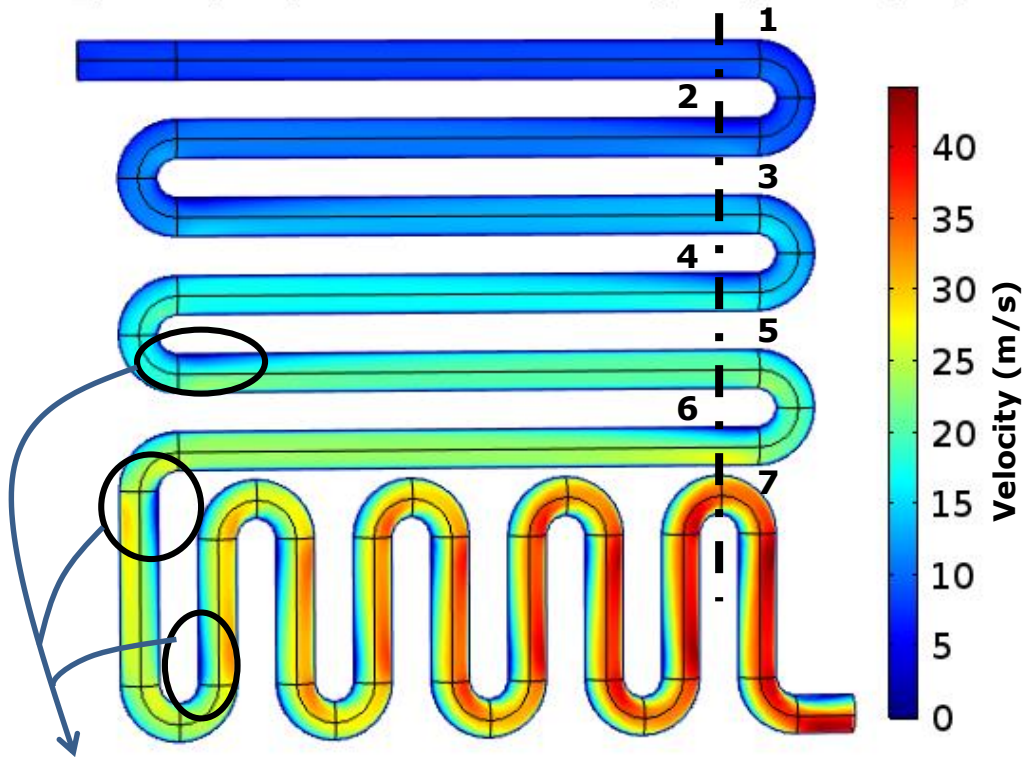
I_heater = 185 A, Slice: Temperature (°C), Arrow: Velocity field



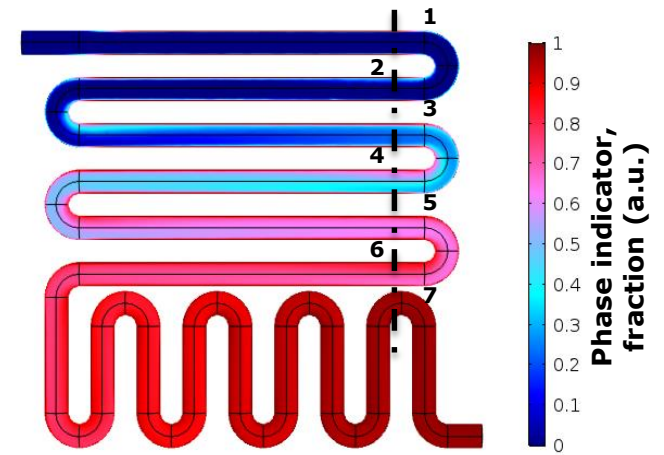
Results: Fluid flow



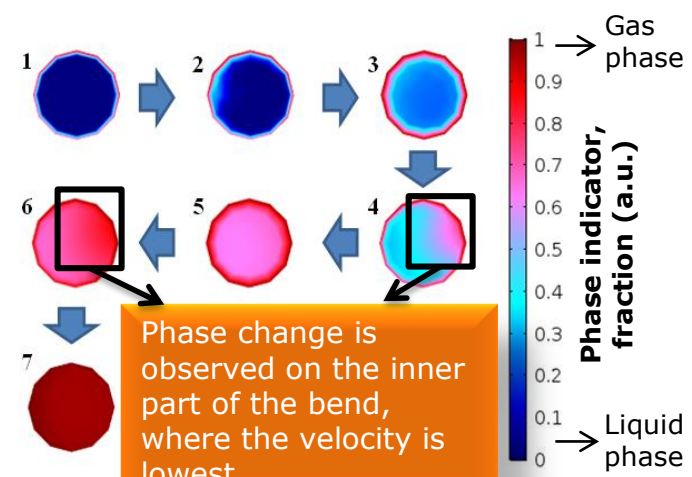
I_heater(277)=185 Slice: Velocity magnitude (m/s)



I_heater = 185 A, Slice: Phase indicator (-)



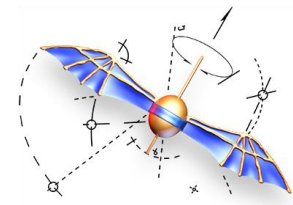
I_heater = 185 A, Slice: Phase indicator (-)



Phase change is observed on the inner part of the bend, where the velocity is lowest

Pressure drop around a bend → velocity difference.
Heat transfer to the fluid increases with lower velocity → phase transition is observed more around bends

Conclusions



- Multiphase flow was approximated as a single flow
- Modeling concept was created for the phase change behavior of an aerosol containing a binary mixture using apparent heat capacity formulation.
- Effective material properties of the aerosol is defined and integrated in the model as molar basis.
- Serpentine meander channels ensure aerosol mixing (homogeneity) and increase the heat transfer
- Due to phase change and the poor thermal conductivity of aerosol gas, more heat and/or mixing is required near phase change region

Thank you
for your attention



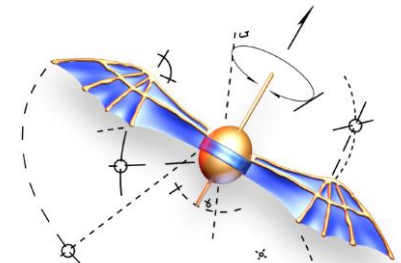
EUROPÄISCHE UNION
Investition in unsere Zukunft
Europäischer Fonds
für regionale Entwicklung



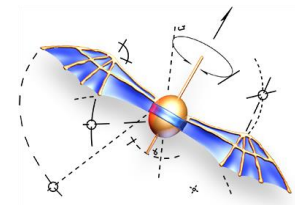
EFRE.NRW
Investitionen in Wachstum
und Beschäftigung

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Parameters



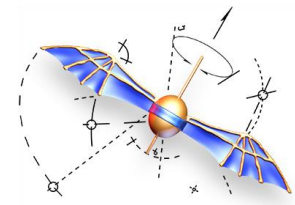
➤ **Fluid properties:**

- Volumetric flow rate of $\text{H}_2\text{O}_{2(\text{aq})}$ (35%): 1000 $\mu\text{L/s}$
- Volumetric flow rate of air: 2 m^3/h
- Inlet fluid velocity: 7 m/s
- Inlet fluid temperature: 20 $^\circ\text{C}$

➤ **Heating element:**

- Set current: 1-185 A
- Thickness of the heating element: 0.1 mm

Heating



Two-stage heating strategy was adopted:

1. Initial heating from main current 0-150 A (equivalent to: 0-1700 W) → initial phase change is observed
2. Low thermal conductivity of aerosol gas after phase change → an auxiliary heating switched around 150 A

