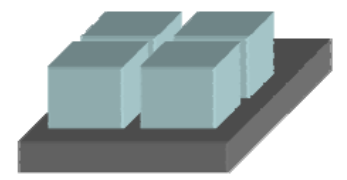
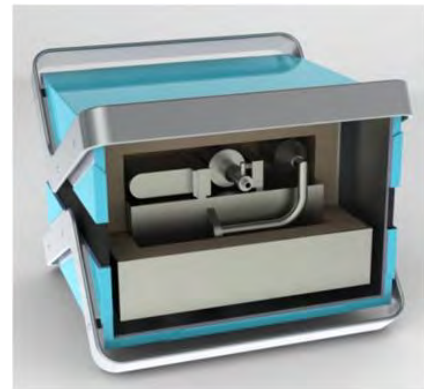

Multiphysics Simulation of an Anode-supported Micro-tubular Solid Oxide Fuel Cell (SOFC)

Gregor Ganzer, Wieland Beckert, Thomas Pfeifer, and Alexander Michaelis
Fraunhofer-Institut für Keramische Technologien und Systeme, Dresden



SOFC systems developed at IKTS

Different power rates



Tubular
SOFC

LPG
SOFC

Natural gas
SOFC

Biogas
SOFC

Multiple
CFY-Stacks

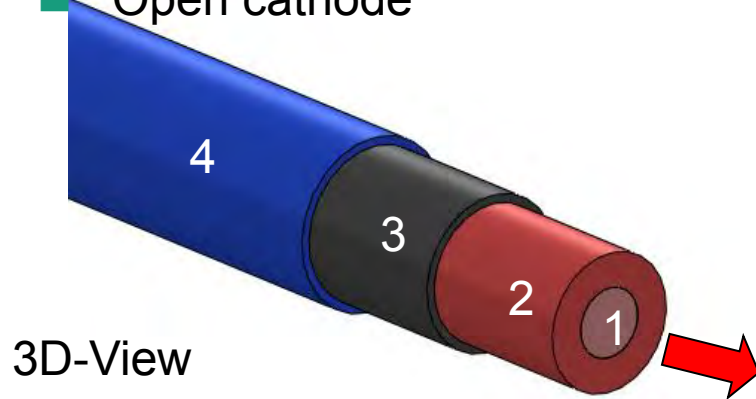
AGENDA

- Model setup
- Results
- Conclusion

Model of a tubular SOFC

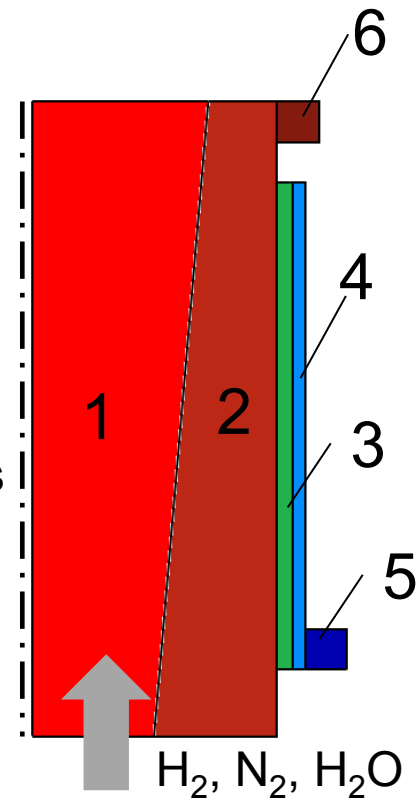
Layout of a micro-tubular SOFC

- Specific advantages:
 - Fast thermal startup
 - High thermal stability
- Typical length in a range of some cm
- Anode Supported Cell (ASC)
- Open cathode



Axisymmetric Sketch (scaled)

- 1 Anode channel
- 2 Porous anode
- 3 Electrolyte
- 4 Porous cathode
- 5/6 Current collectors



Model setup

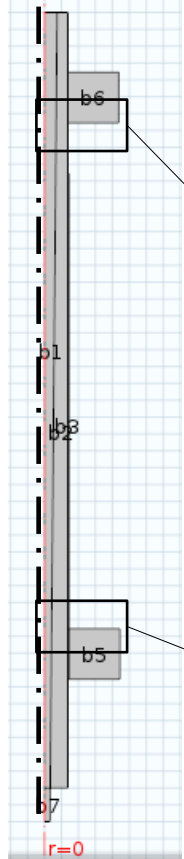
Model development in COMSOL 4.2

- Axisymmetric model of microtubular SOFC
- Parameterized axisymmetric geometry of a single cell
- Multiphysics Simulation
 - Anode gas flow (Navier-Stokes equations, laminar)
 - Heat transfer (convection, conduction, radiation to the hotbox)
 - Diffusion (multicomponent Maxwell-Stefan diffusion)
 - Electrochemical submodel
 - Electric conduction
 - Reduced Butler-Volmer kinetics
 - Special treatment of porous zones (effective properties)
- In total seven physical modes

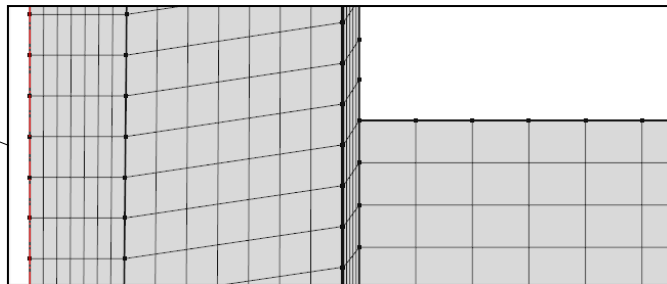
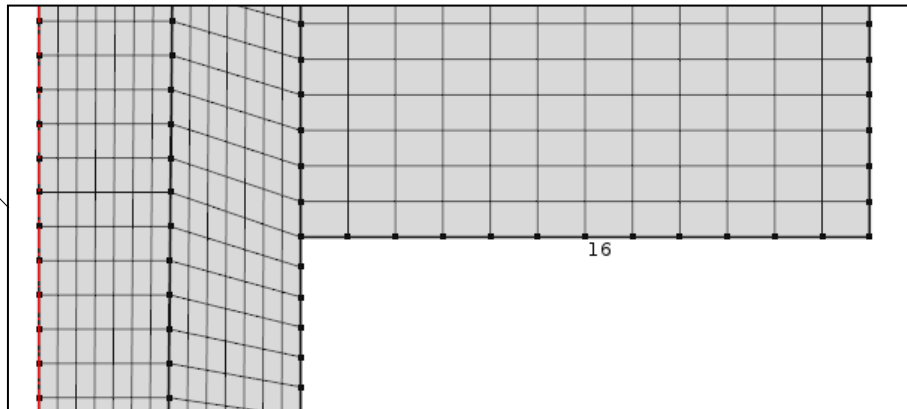
Model setup

Meshing

Geometry:



Mapped mesh with about 5000 quadrilateral elements



Model setup

Electrochemical submodel

- Aim: Description of characteristic polarization behaviour
- Conservation of charge (two electric currents modes)

$$\nabla \cdot (\vec{j}_{\text{ele}}) + \nabla \cdot (\vec{j}_{\text{ion}}) = 0$$

$$\nabla \cdot (-\sigma_{\text{ele}} \nabla \phi_{\text{ele}}) + \nabla \cdot (-\sigma_{\text{ion}} \nabla \phi_{\text{ion}}) = 0$$

- Faraday's law couples molar and current flow:

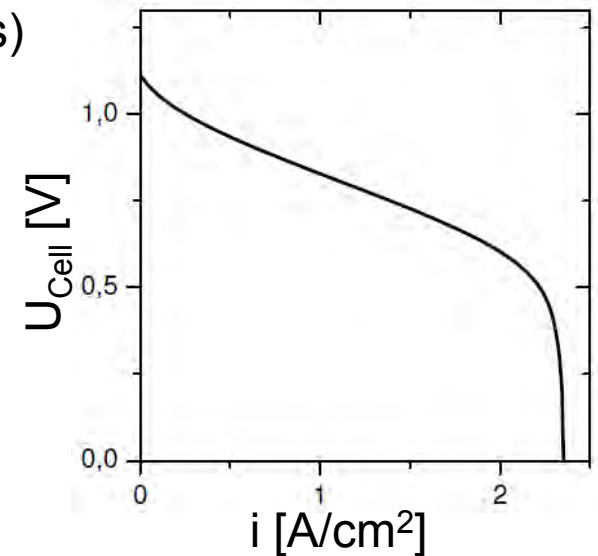
$$\vec{N}_i = \pm \frac{\vec{j}_{\text{ele}}}{nF}$$

- Butler-Volmer equation at electrode/electrolyte interface:

$$i_{\text{BV}} = i_0 \left\{ \exp\left(\frac{\alpha_a F \eta_{\text{act}}}{RT}\right) - \exp\left(-\frac{\alpha_c F \eta_{\text{act}}}{RT}\right) \right\}$$

$$\eta_{\text{act}}^{a,c} = (\phi_{\text{ele}}^{a,c} - \phi_{\text{ion}}^{a,c}) - E_{\text{rev}}^{a,c}$$

$$E_{\text{Nernst}} = E_{\text{rev}}^c - E_{\text{rev}}^a = -\frac{\Delta G}{2F} + \frac{RT}{2F} \ln \left(\frac{x_{\text{H}_2} x_{\text{O}_2}^{0.5}}{x_{\text{H}_2\text{O}}} \right)$$



\vec{j} current density	α symmetry factor	R universal gas constant
σ electric conductivity	F Faraday constant	ΔG Gibbs free energy
ϕ potential	η_{act} activation overpotential	x_i molar fraction
i_0 exchange current density	T temperature	\vec{N} molar flux

Folie 7

Model setup

Mass transport submodel

- Inside the anode channel, multicomponent diffusion for ternary mixture is used:

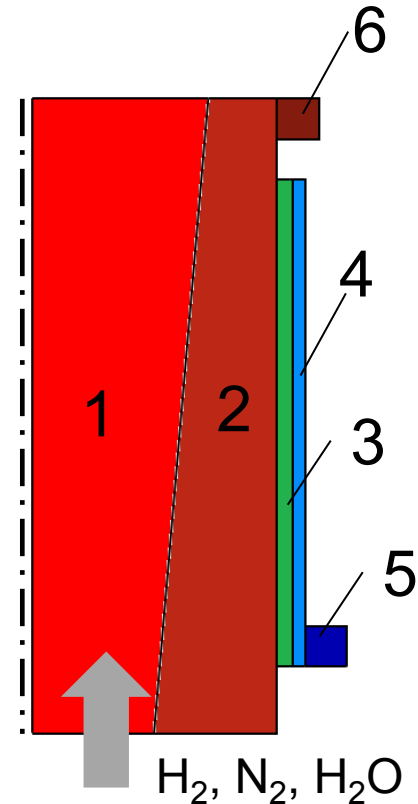
$$\sum_{\substack{j=1 \\ j \neq i}}^N \frac{X_i X_j}{\mathcal{D}_{ij}} \left(\frac{\vec{J}_j}{\rho_j} - \frac{\vec{J}_i}{\rho_i} \right) = \nabla X_i$$

- Inside the porous electrodes, Knudsen diffusion is dominant:

$$D_K^{\text{eff}} = \frac{\varepsilon}{\tau} \cdot \frac{1}{3} d_p \sqrt{\frac{8RT}{\pi M_i}}$$

$$D_K^{\text{eff}} = a_{\text{Knudsen}} \sqrt{\frac{T}{M_i}}$$

Fit parameter



1 Anode channel

2 Porous anode

3 Electrolyte

4 Porous cathode

5/6 Current collectors

H₂, N₂, H₂O

T	Temperature	d_p	Pore diameter	x_i	molar fraction
p	Pressure	R	Gas constant	ρ	density
D_{ij}	Binary diffusion coeff.	ε	Porosity		
\vec{J}_i	Diffusion flux	τ	Tortuosity		

Model setup

Heat sources in SOFCs

- Reversible losses:

$$q''_{rev,a/c} = T \cdot \Delta S_{a/c} \frac{i_{a/c}}{2F}$$

- Irreversible losses:

- Ohmic heating

$$q''' = \sigma \cdot \nabla^2 \phi$$

- Overpotential losses

$$q''_{irrev,a/c} = \eta_{act,a/c} \cdot i_{a/c}$$

- Heat fluxes at outer surface:

$$q'' = q''_{convection} + q''_{radiation} = \frac{Nu \cdot k}{D_h} (T - T_{amb}) + \sigma_0 \cdot \varepsilon_{rad} (T^4 - T_{amb}^4)$$

T Temperature

ΔS Molar entropy change

$i_{a/c}$ Current density at a/c-ele interface

F Faraday constant

σ Electric conductivity

ϕ Electric potential

η_{act} Activation overpotential

k Thermal conductivity

D_h Hydraulic diameter

ε_{rad} Radiative emissivity

σ_0 Boltzmann constant

T_{amb} Ambient temperature (furnace)

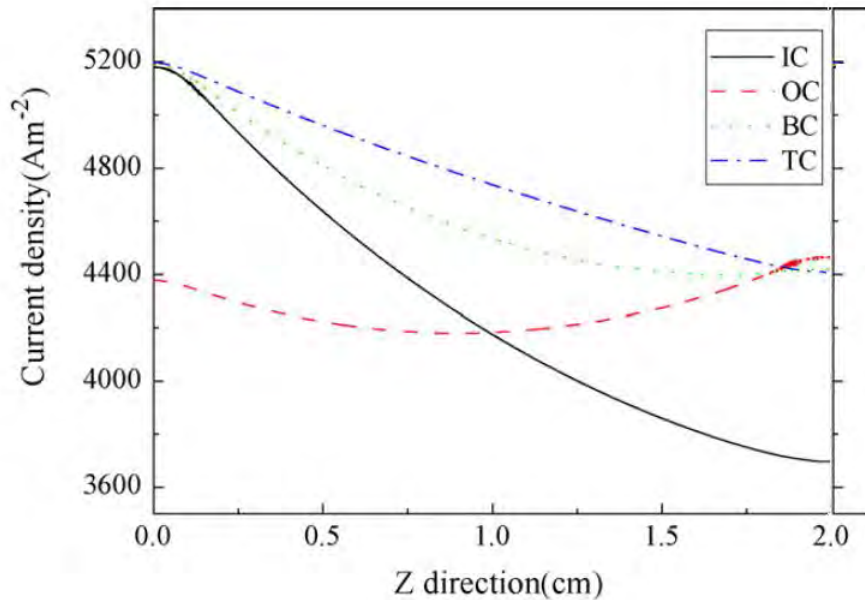
AGENDA

- Model setup
- Results
- Conclusion

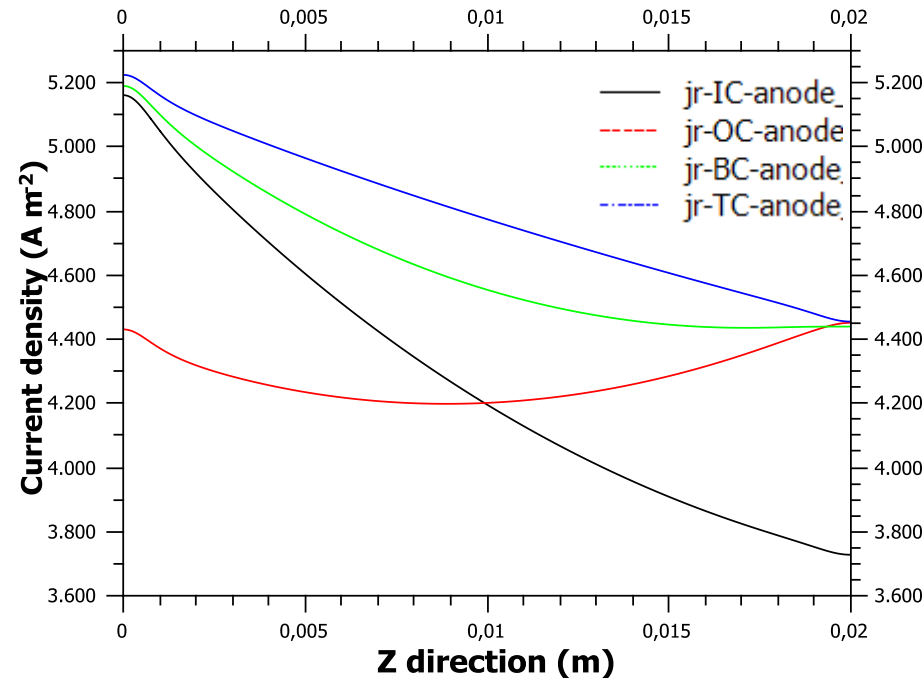
Validation

Comparison to published data

Cui 2007 Model



Own Model



Geometry:

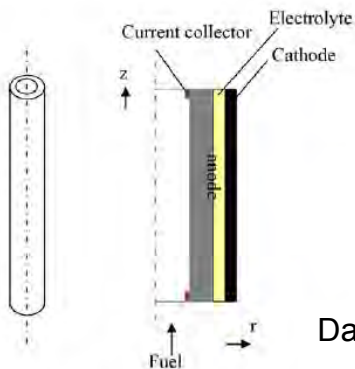


Fig. 1. Schematic diagram of a micro-tubular

Plot of current density at anode/electrolyte interface

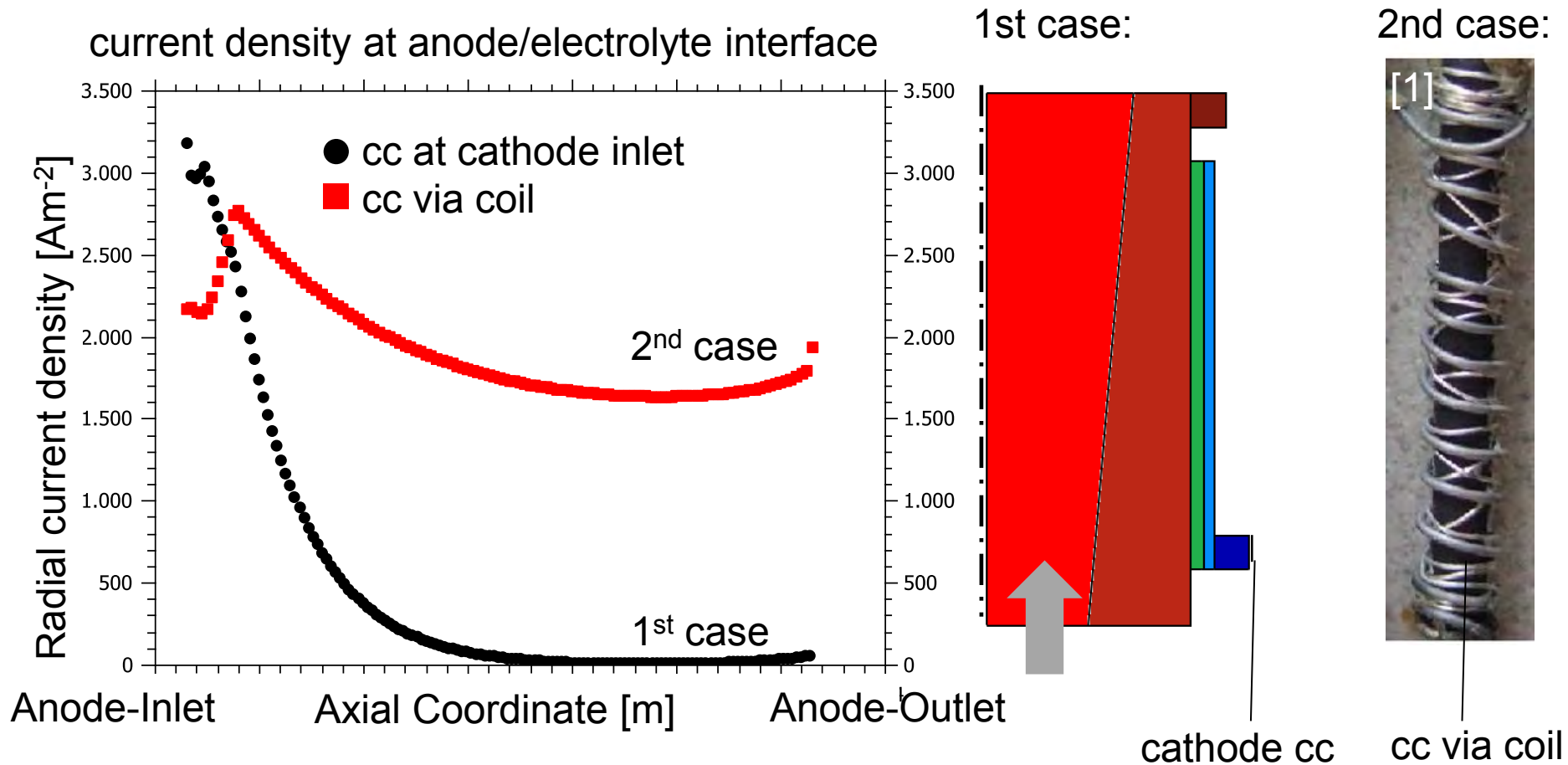
- IC anode inlet current collector
- OC anode outlet current collector
- BC both current collector
- TC total anode current collector

Daan Cui et al., 2007, Journal of Power Sources 174 (2007) 246–254

„Comparison of different current collecting modes of anode supported micro-tubular SOFC through mathematical modeling“

Distribution of current density

Influence of cathodic current collection (cc)



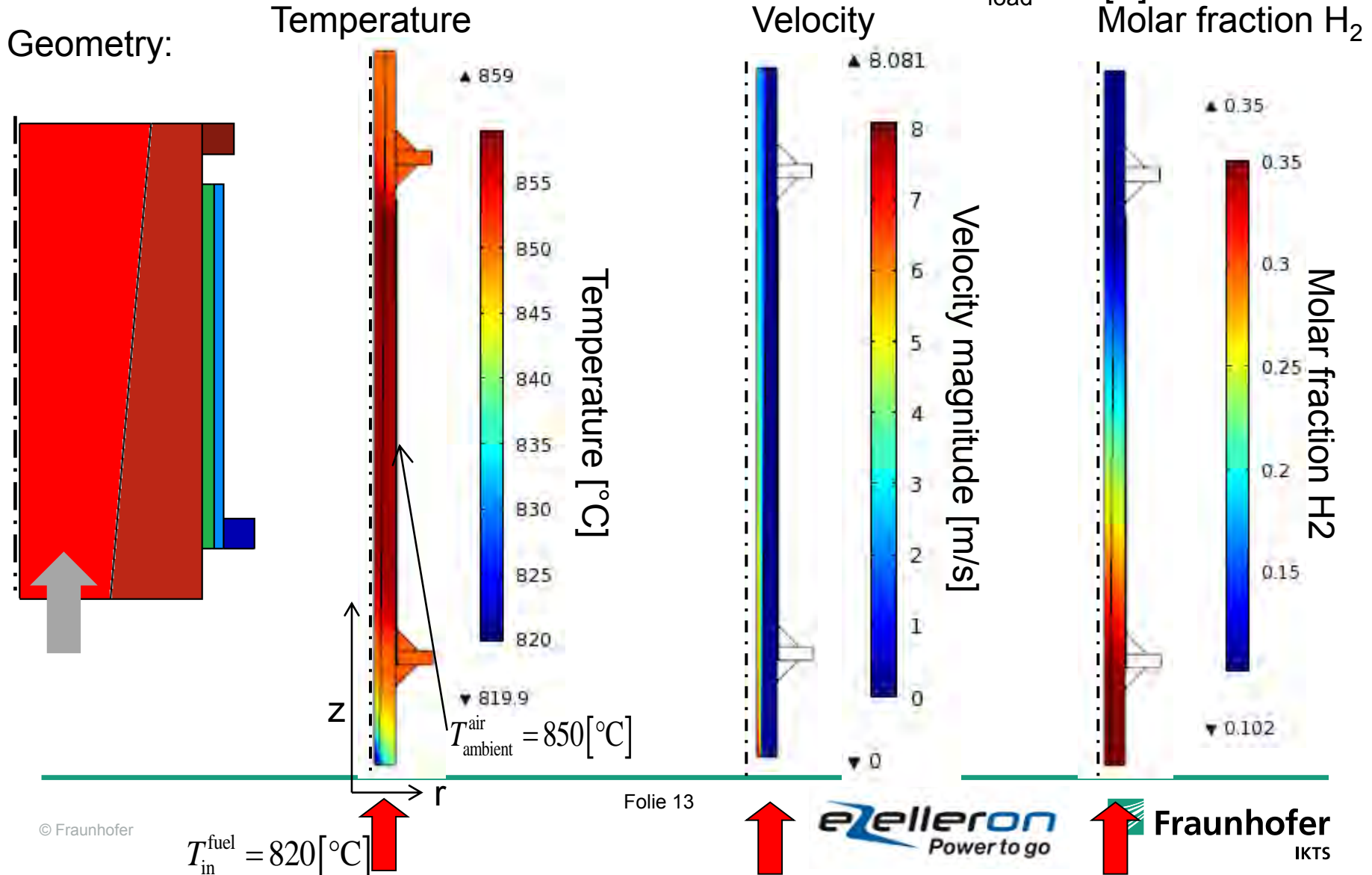
$$U_{\text{Load}} = 0.9 \text{ [V]}$$

Model of a tubular SOFC

Some results

molar fractions:
 $H_2:H_2O:N_2=0.35:0.03:0.62$

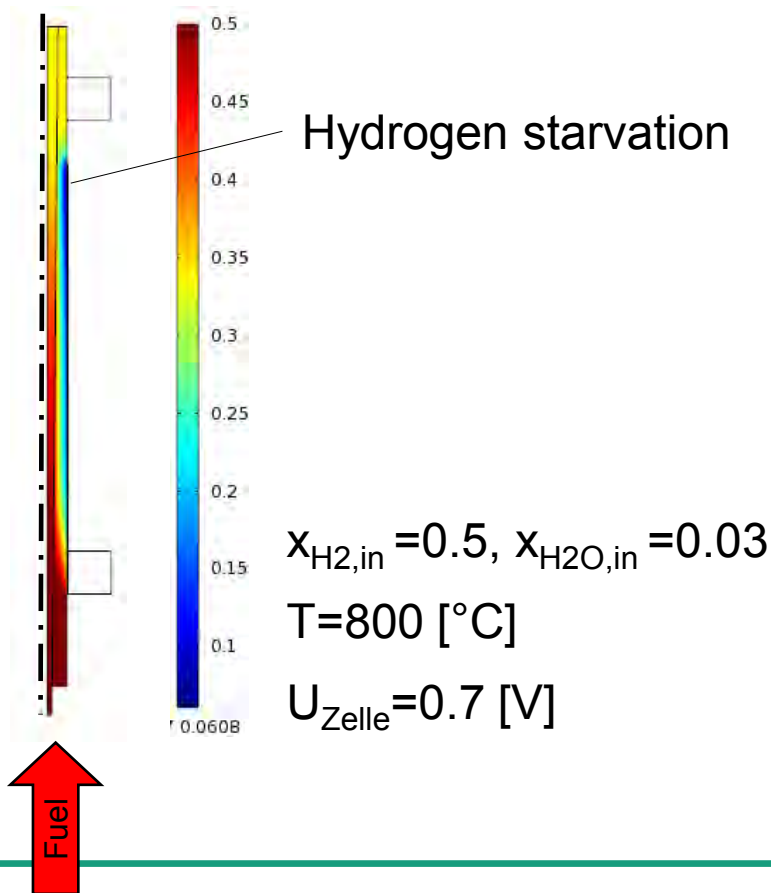
$U_{load}=0.7[V]$



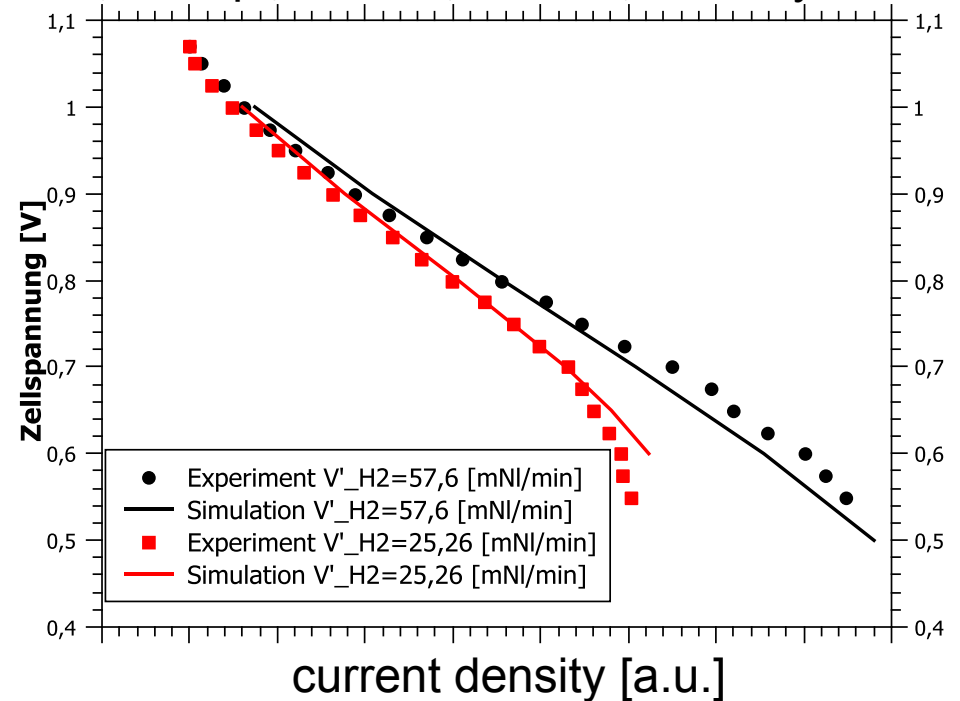
Model of a tubular SOFC

Some results

Hydrogen mole fraction



Cell potential vs. current density



AGENDA

- Model setup
- Results
- Conclusion

Conclusion

- Multiphysics simulations help to understand internal phenomena
- Comparison of different current collection modes
- Influence of mass transport shown

- In progress:
 - Transient simulations
 - Variation of geometric parameters

THANK YOU FOR YOUR ATTENTION!

WWW.IKTS.FRAUNHOFER.DE

